## Formula/Conversion Table

 for Water Treatment Plant and Water Distribution Systems| 1 foot = 12 inches | $1 \mathrm{MGD}=1.55 \mathrm{cfs}$ | 1 grain / gal $=17.1 \mathrm{mg} / \mathrm{L}$ | 1 minute $=60$ seconds |
| :---: | :---: | :---: | :---: |
| 1 yard $=3$ feet | $1 \mathrm{cu} . \mathrm{yd} .=27 \mathrm{cu} . \mathrm{ft}$. | 1 gram $=1,000 \mathrm{mg}$ | 1 hour $=60$ minutes |
| 1 meter $=3.28$ feet | $1 \mathrm{cu} . \mathrm{ft} .=7.48 \mathrm{gal}$ | $1 \mathrm{~kg}=1,000 \mathrm{gram}$ | 1 day $=1,440 \mathrm{~min}$ |
| 1 mile $=5,280$ feet | $1 \mathrm{gal}=8.34 \mathrm{lbs}$ | 1 liter $=1,000 \mathrm{ml}$ | $1 \%=10,000 \mathrm{mg} / \mathrm{L}$ |
| 1 sq. ft. $=144$ sq. in. | $1 \mathrm{cu} . \mathrm{ft} .=62.4 \mathrm{lbs}$ | $1 \mathrm{gal}=3.785$ liters | $1 \mathrm{mg} / \mathrm{l}=1 \mathrm{ppm}$ |
| 1 acre $=43,560$ sq. ft. | $1 \mathrm{~kg}=2.2 \mathrm{lbs}$ | $1 \mathrm{psi}=2.31 \mathrm{ft}$. of water head | $1 \mathrm{hp}=0.746 \mathrm{~kW}$ |
| $1 \mathrm{acre-ft}=43,.560 \mathrm{cu} . \mathrm{ft}$. | $1 \mathrm{lb} .=454 \mathrm{~g}$ | 1 ft . of water head $=0.433 \mathrm{psi}$ | $1 \mathrm{hp}=33,000 \mathrm{ft} . \mathrm{lbs} / \mathrm{min}$ |
| 1 acre-ft. $=325,829$ gallons |  |  | $1 \mathrm{~kW}=1,000$ Watts |
| Legend: L = length $\quad \mathrm{W}=$ | width $\quad \mathrm{H}=$ height | $\mathrm{R}=$ radius $\quad \mathrm{D}=$ diameter | $\pi=3.14 \quad \mathrm{~g}=8$ |

## Alkalinity Concepts

Phenolphthalein Alkalinity, $\mathrm{mg} / \mathrm{L}$ as $\mathrm{CaCO}_{3}=$ (Titrant Volume A, ml) (Acid Normality) $(50,000)$ Sample Volume, ml

Total Alkalinity, $\mathrm{mg} / \mathrm{L}$ as $\mathrm{CaCO}_{3}=$
(Titrant Volume B, ml) (Acid Normality) $(50,000)$
Sample Volume, ml
Alkalinity Relationships: Alkalinity, $\mathrm{mg} / \mathrm{l}{\text { as } \mathrm{CaCO}_{3}}$

| Result of <br> Titration | Bicarbonate <br> Alkalinity as <br> $\mathrm{CaCO}_{3}$ | Carbonate <br> Alkalinity as <br> $\mathrm{CaCO}_{3}$ | Hydroxide <br> Alkalinity as <br> $\mathrm{CaCO}_{3}$ |
| :--- | :---: | :---: | :---: |
| $\mathrm{P}=0$ | T | 0 | 0 |
| $\mathrm{P}<1 / 2 \mathrm{~T}$ | $\mathrm{~T}-2 \mathrm{P}$ | 2 P | 0 |
| $\mathrm{P}=1 / 2 \mathrm{~T}$ | 0 | 2 P | 0 |
| $\mathrm{P}>1 / 2 \mathrm{~T}$ | 0 | $2(\mathrm{~T}-\mathrm{P})$ | $2 \mathrm{P}-\mathrm{T}$ |
| $\mathrm{P}=\mathrm{T}$ | 0 | 0 | T |

Key: P - phenolphthalein alkalinity; T-total alkalinity

## Area, Circumference and Volume

## Area, square feet $\left(\mathrm{ft}^{2}\right)$

Circle: $A=3.14 \times R^{2}$ or $A=0.785 \times D^{2}$
Cylinder, (total outer surface area): $A=\left(2 \times 3.14 \times R^{2}\right)+3.14 \times D \times H$ or $A=\left(2 \times 0.785 \times D^{2}\right)+(3.14 \times D \times H)$ Cylinder (pipe): $A=3.14 \times D \times L$
Square or Rectangle: $A=L \times W$

## Circumference (Perimeter), linear feet

Circle $=3.14 \times$ D
Rectangle $=(2 \times \mathrm{L})+(2 \times \mathrm{W})$
Volume, cubic feet $\left(\mathrm{ft}^{3}\right)$ :
Cylinder: $\mathrm{V}=3.14 \times \mathrm{R}^{2} \times \mathrm{H}$ or $\mathrm{V}=0.785 \times \mathrm{D}^{2} \times \mathrm{H}$
Rectangle: $\mathrm{V}=\mathrm{L} \times \mathrm{W} \times \mathrm{H}$

Average $($ arithmetic mean $)=$
Sum of All Terms or Measurements Number of Terms or Measurements

Sum of All Averages

Annual Running Average $=$

## Chemical Feed, Mixing and Solution Strengths

Chemical Feed, lbs/day = (Dry Chemical Feeder)
(Dry Chemical, g) (60 min/hr.) (24 hr./day)
( $454 \mathrm{~g} / \mathrm{lb}$.) (Time, min )

Chemical Feed, lbs/day $=\quad$ (Polymer Conc., $\mathrm{mg} / \mathrm{l})$ (Volume Pumped, ml$)(60 \mathrm{~min} / \mathrm{hr}$.) ( $24 \mathrm{hr} . /$ day $)$
(Polymer Feeder)
(Time Pumped, min ) $(1,000 \mathrm{mg} / \mathrm{I})(1,000 \mathrm{mg} / \mathrm{gm})(454 \mathrm{gm} / \mathrm{lb}$.

Chemical feed pump setting, \% stroke $=\quad \frac{\text { Desired feed flow, gpd }}{\text { Maximum feed flow, gpd }} \times 100 \%$

Chemical Feed Pump Setting, $\mathrm{mL} /$ minute $=$
(Flow, MGD) (Dose, $\mathrm{mg} / \mathrm{L}$ ) (3.785 L/gal) (1,000,000 gal/MG)
(Liquid alum, $\mathrm{mg} / \mathrm{ml})(1,440 \mathrm{~min} /$ day $)$

Hypochlorite Strength, $\%=\frac{\text { Chlorine required, lbs/day }}{\text { (Hypochlorite solution needed, gal/day) (8.34 lbs./gal) }} \times 100 \%$
Lbs. of Chemical $=\quad$ (amount of solution needed, gal) (solution strength, as a decimal) (8.34 lbs/gal)
Liquid Polymer, gal $=\frac{\text { (Polymer Solution, \%) (gal of solution) }}{\text { Supplied }}$ Supplied Liquid Polymer, \%

Mixture Strength, \% = (Amount 1, gals) (Strength 1, \%) + (Amount 2, gals) (strength 2, \%)
(Amount 1, gals) + (Amount 2, gals)

Polymer Solution, \% = $\frac{\text { (Dry Polymer, Ibs) (100\%) }}{\text { (Dry Polymer, Ibs + Water, Ibs) }}$

Water added for hypochlorite sol'n, gal =
(hypo, gal) (hypo,\%) - (hypo, gal) (desired hypo,\%) Desired hypo, \%

Potassium Permanganate Dose, $\mathrm{mg} / \mathrm{L}=(0.2 \times$ Iron content, $\mathrm{mg} / \mathrm{L})+(2.0 \times$ Manganese content, $\mathrm{mg} / \mathrm{L})$

## Demineralization

Membrane Area, sq ft = (Number of Vessels) (Number of Elements per Vessel) (Surface Area per Element)

Mineral Rejection, $\%=\left(1-\frac{\text { Product TDS Concentration, } \mathrm{mg} / \mathrm{L}}{\text { Feedwater TDS Concentration, } \mathrm{mg} / \mathrm{L}}\right) \times 100 \%$

Recovery, $\%=\frac{\text { Product Flow, MGD }}{\text { Feed Flow, MGD }} \times 100 \%$

## Detention Time

Detention Time, days $=\frac{\text { Tank Volume, gallons }}{\text { Flow Rate, gal/day }} \quad \begin{aligned} & \text { Note: for detention time in hours, multiply by } 24 \text { hrs/day } \\ & \text { For detention time in minutes, multiply by } 1,440 \mathrm{~min} / \text { day }\end{aligned}$

## Disinfection

Chlorine Demand, $\mathrm{mg} / \mathrm{L}=$ Chlorine Dosage, $\mathrm{mg} / \mathrm{L}-$ Chlorine Residual, $\mathrm{mg} / \mathrm{L}$
Chlorine Dosage, $\mathrm{mg} / \mathrm{L}=\quad$ Chlorine Demand, $\mathrm{mg} / \mathrm{L}+$ Chlorine Residual, $\mathrm{mg} / \mathrm{L}$
Chlorine Residual, $\mathrm{mg} / \mathrm{L}=$ Chlorine Dosage, $\mathrm{mg} / \mathrm{L}$ - Chlorine Demand, $\mathrm{mg} / \mathrm{L}$
CT calculation, time $=($ Disinfectant Residual Concentration, $\mathrm{mg} / \mathrm{L})$ (Time) Time units must be compatible

## Electrical

$\operatorname{Amps}(\mathrm{I})=\frac{\operatorname{Volts}(\mathrm{E})}{\operatorname{Ohms}(\mathrm{R})}$
Electromotive Force (EMF), volts = (Current, amps) (Resistance, ohms) or E $=1 \times \mathrm{R}$
Power, kilowatts (3 phase AC circuit) $=\frac{(E, \text { volts) (I, amps) (Power Factor) (1.73) }}{1,000 \text { watts/kilowatt }}$

Power, kilowatts (single phase AC circuit) $=\frac{(E, \text { volts) (I, amps) (Power Factor) }}{1,000 \text { ( }}$ 1,000 watts/kilowatt

Power, watts (DC circuit) $=(\mathrm{E}$, volts) (I, amps) or $\mathrm{P}=\mathrm{ExI} \longrightarrow$


Power Output, horsepower $=\frac{\text { (Power Input, Kw x Efficiency, \%) }}{0.746 \mathrm{Kw} / \mathrm{Hp}} \times 100 \%$
Power Requirements, kW-hr = (Power, kilowatts) (Time, hours)
Feed Rate, 100\% chlorine
Feed Rate, lbs/day = (Dosage, mg/L) (Flow, MGD) (8.34 lbs/gal)


Using the Davidson Pie Chart

- To find the quantity above the horizontal line: Multiply the 3 pie wedges below the line together. Next, divide by the \% purity as a decimal (i.e., $65 \%=0.65$ ).
- To solve for one of the pie wedges below the horizontal line: Divide the 2 bottom pie wedges into the quantity of Ibs above the horizontal line. Next, multiply by the $\%$ purity as a decimal (i.e., $65 \%=0.65$ ).
- The given units must match the units shown in the pie wheel.
- Dose $=\mathrm{mg} / \mathrm{L}$ or PPM

Calcium Hypochlorite $(\mathrm{CaOCl})$, lbs. $=\frac{\text { Pure chlorine required, } \mathrm{lbs} / \text { day }}{\mathrm{CaOCl} \% \text { Purity, as decimal }} \times 100 \%$
Sodium Hypochlorite $(\mathrm{NaOCl})$, gals. $=\frac{\text { Pure chlorine required, lbs/day }}{(\mathrm{NaOCl} \% \text { purity as decimal) }(8.34 \mathrm{lbs} / \mathrm{gal})} \times 100 \%$

## Filtration

Backwash Rise Rate, inches $/ \mathrm{min}=\frac{\text { (Backwash Rate, gpm } / \mathrm{sq} . \mathrm{ft} .)(12 \mathrm{in} / \mathrm{ft})}{7.48 \mathrm{gal} / \mathrm{cu} . \mathrm{ft} .}$
Backwash Pumping Rate, gal/min $=\quad$ (Backwash Rate, gpm/sq. ft.) (Filter Surface Area, sq. ft.)
Backwash Water Required, gal $=($ Backwash Flow, gpm) $($ Backwash Time, min $)$
Backwash Water Used, \% = $\frac{\text { Backwash Water, gal }}{\text { Water Filtered, gal }} \times 100 \%$

Filtration Rate or Backwash Rate, $\mathrm{gpm} / \mathrm{sq} \mathrm{ft}=\frac{\text { Flow Rate, } \mathrm{gpm}}{\text { Filter Surface Area, } \mathrm{sq} \mathrm{ft}}$

Hydraulic or Surface Loading Rate, gpd/sq ft $=\frac{\text { Total Flow Applied, gpd }}{\text { Surface Area, sq ft }}$

Unit Filter Run Volume, gal/sq ft $=\frac{\text { Total Volume Filtered, gal }}{\text { Filter Surface Area, } \mathrm{sq} \mathrm{ft}}$

Unit Filter Run Volume, gal/sq ft = (Filtration Rate, gpm/sq. ft.) (Filter Run, hr) (60 min/hr)
Flow Rates and Velocity (pipeline, channel or stream)
Flow Rate, cfs = (Area, sq. ft.) (Velocity, ft/sec) or $\mathrm{Q}=\mathrm{V} \times \mathrm{A}$


Where:
Q = flow rate, cfs
$\mathrm{V}=$ velocity, fps
$\mathrm{A}=$ area, $\mathrm{ft}^{2}$

Flow Rate, $\mathrm{gpm}=($ Area, sq. ft. $)($ Velocity, $\mathrm{ft} / \mathrm{sec})(7.48 \mathrm{gal} / \mathrm{cu} \mathrm{ft})(60 \mathrm{sec} / \mathrm{min})$ or $\mathrm{Q}=\mathrm{V} \times \mathrm{A} \times 7.48 \times 60$

Velocity, $\mathrm{fps}=\frac{\text { Flow Rate, } \mathrm{cfs}}{\text { Area, } \mathrm{sq} \mathrm{ft}}$ or $\frac{\text { Distance, } \mathrm{ft}}{\text { Time, seconds }}$

## Fluoridation

Feed Rate, lbs/day =
(Dosage, mg/L) (Flow, MGD) (8.34 lbs/gal)
(Fluoride Sol'n, as a decimal) (Fluoride Purity, as a decimal)

Feed Rate, gpd =
Feed Rate, Ibs/day
Chemical Solution, Ibs/gal
Feed Rate, lbs/day $=\quad \frac{\text { Fluoride, lbs/day }}{\text { Fluoride, lbs/lb of commercial chemical }}$

Fluoride lon Purity, \% = $\frac{\text { Molecular Weight of Fluoride }}{\text { Molecular Weight of Compound }} \times 100 \%$

## Flushing Time

Flushing Time, sec $=\frac{\text { Volume, cu ft }}{\text { Flow, } \mathrm{cfs}} \quad$ or $\quad$ (Length of Pipeline, ft ) (Number of Flushing Volumes)

## Laboratory

Dilute to $\mathrm{ml}=$

$$
\frac{(\text { Actual Weight, gm) }(1,000 \mathrm{ml})}{\text { Desired Weight, gm }}
$$

Langelier Saturation Index (L.S.I.) $=\mathrm{pH}-\mathrm{pH}_{\mathrm{s}}$

## Leakage and Pressure Testing Pipelines

Leakage, gpd $=\quad \frac{\text { Volume, gal }}{\text { Time, days }}$
Asbestos Cement (AC) or Ductile Iron (DI) Pipe, gpd/mi-in = $\frac{\text { Leak Rate, gpd }}{\text { (length, miles) (Diameter, in) }}$
Plastic Pipe Leakage, gph/100 joints $=\frac{\text { Leak Rate, } \mathrm{gph}}{\text { (Number of Joints } \div 100 \text { ) }}$
Test Pressure, psi $=$ Normal Pressure $+50 \%$ or 150 psi, whichever is greater

## Loading

Weir Overflow Rate, gpd/ft $=\frac{\text { Total Flow, gpd }}{\text { Length of Weir, } \mathrm{ft}}$

## Parts per million (PPM) or milligrams per liter, (mg/L)

Dosage, PPM or $\mathrm{mg} / \mathrm{L}=\frac{\text { Pounds of Chemical, Ibs }}{\text { (Water Volume, MG) (8.34 lbs/gal) }}$

## Pressure and Head

Head (Height of Water), $\mathrm{ft}=($ Pressure, psi$)(2.31 \mathrm{ft} / \mathrm{psi}) \quad$ or $\quad$ Head (Height of Water), $\mathrm{ft}=\frac{\text { Pressure, } \mathrm{psi}}{0.433 \mathrm{psi} / \mathrm{ft}}$
Pressure, $\mathrm{psi}=\frac{\text { Head, } \mathrm{ft}}{2.31 \mathrm{ft} / \mathrm{psi}}$ or Pressure, $\mathrm{psi}=($ Head, ft$)(0.433 \mathrm{psi} / \mathrm{ft})$

## Pumps, Motors and Horsepower

Water Horsepower $($ WHP $)=\frac{(\text { Flow, gpm })(\text { Head, } \mathrm{ft})}{3,960}$
Brake Horsepower $(\mathrm{BHP})=\frac{(\text { Flow, } \mathrm{gpm})(\text { Head, } \mathrm{ft})}{(3,960)(\text { Pump Efficiency as decimal) }}$
Motor Horsepower (MHP) $=\frac{\text { (Flow, gpm) (Head, ft) }}{(3,960)(\text { Pump Efficiency as decimal) (Motor Efficiency as decimal) }}$

Pumping Rate, gpm $=\quad \frac{\text { Volume, gal }}{\text { Time, } \mathrm{min}}$

Total Dynamic Head, $\mathrm{ft}=\quad$ Static Head, $\mathrm{ft}+$ Discharge Head, $\mathrm{ft}+$ Friction Loss, ft

Wire-to-Water Efficiency, $\%=\frac{\text { Water Horsepower, WHP }}{\text { Power Input, (Brake Hp or Water Hp) }} \times 100 \%$
Wire-to-Water Efficiency, $\%=\frac{\text { (Flow, gpm) (Total Dynamic Head, ft) }}{\text { (Voltage, volts) (Current, amps) (5.308) }} \times 100 \%$

Kilowatt-hr/day $=$ (Motor, Hp) (Motor Run Time, hr/day) (0.746 kW/Hp)

## Softening Processes

## Hardness

Total Hardness, $\mathrm{mg} / \mathrm{l}$ as $\mathrm{CaCO}_{3}=$ Calcium Hardness, $\mathrm{mg} / \mathrm{l}$ as $\mathrm{CaCO}_{3}+$ Magnesium Hardness, $\mathrm{mg} / \mathrm{l}$ as $\mathrm{CaCO}_{3}$
If alkalinity is greater than total hardness:
Carbonate Hardness, $\mathrm{mg} / \mathrm{l}$ as $\mathrm{CaCO}_{3}=$ Total Hardness, $\mathrm{mg} / \mathrm{l}$ as $\mathrm{CaCO}_{3}$ and,
Noncarbonate Hardness, $\mathrm{mg} / \mathrm{l}$ as $\mathrm{CaCO}_{3}=0$
If alkalinity is less than total hardness:
Carbonate Hardness, $\mathrm{mg} / \mathrm{l}$ as $\mathrm{CaCO}_{3}=$ Amount of total hardness up to the Total Alkalinity, $\mathrm{mg} / \mathrm{l}$ as $\mathrm{CaCO}_{3}$, or
Noncarbonate Hardness, $\mathrm{mg} / \mathrm{l}$ as $\mathrm{CaCO}_{3}=$ Total Hardness, $\mathrm{mg} / \mathrm{l}$ as $\mathrm{CaCO}_{3}-$ Total Alkalinity, $\mathrm{mg} / \mathrm{l}$ as $\mathrm{CaCO}_{3}$

## Lime / Soda Ash Softening

Note: If hydrated lime $\left(\mathrm{Ca}(\mathrm{OH})_{2}\right)$ is used instead of quicklime ( CaO ), substitute 74 for 56 in equations below.
Lime Feed, $m g / L=\frac{(A+B+C+D)(1.15)}{\text { Purity of Lime, as a decimal }}$

| $A=$ Carbon dioxide $\left(\mathrm{CO}_{2}\right)$ in source water: | $\mathrm{mg} / \mathrm{l}$ as $\mathrm{CO}_{2}$ | $\mathrm{x}(56 / 44)$ |
| :--- | :--- | :--- |
| $B=$ Bicarbonate alkalinity removed in softening: | source water, $\mathrm{mg} / \mathrm{l}$ as $\mathrm{CaCO}_{3}-$ softened water, $\mathrm{mg} / \mathrm{l}$ as $\mathrm{CaCO}_{3}$ | $\mathrm{x}(56 / 100)$ |
| $C=$ Hydroxide alkalinity in softener effluent: | $\mathrm{mg} / \mathrm{l}$ as $\mathrm{CaCO}_{3}$ | $\times(56 / 100)$ |
| $D=$ Magnesium removed in softening: | source water $\mathrm{Mg}^{2+}, \mathrm{mg} / \mathrm{l}$ - softened water $\mathrm{Mg}^{2+}, \mathrm{mg} / \mathrm{l}$ | $\mathrm{x}(56 / 24.3)$ |

Excess Lime, mg/I = $(A+B+C+D)(0.15)$
Soda Ash, dosage to remove noncarbonated hardness:
Soda Ash $\left(\mathrm{Na}_{2} \mathrm{CO}_{3}\right)$ Feed, $\mathrm{mg} / \mathrm{I}=\left(\right.$ Noncarbonate Hardness, $\mathrm{mg} / \mathrm{I}$ as $\left.\mathrm{CaCO}_{3}\right)(106 / 100)$
Carbon Dioxide, dosage to recarbonate:
Total $\mathrm{CO}_{2}$ Feed, $\mathrm{mg} / \mathrm{I}=($ excess lime, $\mathrm{mg} / \mathrm{I})(44 / 56)+\left(\mathrm{Mg}^{2+}\right.$ residual, $\left.\mathrm{mg} / \mathrm{I}\right)(44 / 58.3)$

Lime Feeder Setting, Ibs/day = (Flow, MGD) (Dose, mg/l) (8.34 lbs/gal)

Feed Rate, lbs/min =

## Feeder Setting, Ibs/day

1,440 min/day

## Ion Exchange Softening

Hardness, grains/gallon $=\frac{(\text { Hardness, } \mathrm{mg} / \mathrm{l})(1 \text { grain } / \text { gallon })}{17.1 \mathrm{mg} / \mathrm{l}}$
Exchange Capacity, grains $=($ Media Volume, cu ft $)($ Removal Capacity, grains/cu ft $)$
Water Treated, gal $=\frac{\text { Exchange capacity, grains }}{\text { Hardness Removed, grains/gallon }}$
Unit Operating Time, hrs $=\frac{\text { Water Treated, gallons }}{(\text { Avg Daily Flow, } \mathrm{gpm})(60 \mathrm{~min} / \mathrm{hr})}$
Bypass Flow, gpd = $\frac{\text { (Total Flow, gpd) (Desired Finished Water Hardness, gpg) }}{\text { Source Water Hardness, gpg }}$
Bypass Water, gals $=\quad\left(\begin{array}{l}\text { (Softener Capacity, gal) }(\text { Bypass Flow, gpd }) \\ \text { Softener Flow, gpd }\end{array}\right.$
Total Flow, gallons = Softener Capacity, gal + Bypass Water, gal

## Temperature Conversions

Degrees Celsius, ${ }^{\circ} \mathrm{C}=\left({ }^{\circ} \mathrm{F}-32\right)(0.555)$ or $\frac{\left({ }^{\circ} \mathrm{F}-32\right)}{1.8}$
Degrees Fahrenheit, ${ }^{\circ} \mathrm{F}=\left({ }^{\circ} \mathrm{C} \times 1.8\right)+32$

## Turbidity

Removal Percentage, $\%=\frac{\text { (Influent Turbidity - Effluent Turbidity) }}{\text { Influent Turbidity }} \times 100 \%$

## Water Loss

Unaccounted For Water, $\%=\frac{\text { (Water Produced, gals }- \text { Water Billed, gals) }}{\text { Water Produced, gals }} \times 100 \%$

## Water Production

Gallons per Capita/Day $=\frac{\text { Volume of Water Produced, gpd }}{\text { Population Served }}$

## Water Treatment Plant \% capacity

Capacity, $\%=\frac{\text { Average Daily Flow, MGD }}{\text { Plant Design Capacity, MGD }} \times 100 \%$

## Abbreviations:

| cfs | Cubic feet per second | m | Meter |
| :--- | :--- | :--- | :--- |
| DO | Dissolved oxygen | mg | Milligrams |
| ft | Feet | $\mathrm{mg} / \mathrm{L}$ | Milligrams per liter |
| fps | Feet per second | lbs | Pounds |
| GFD | Gallons per day per square foot | MGD | Million gallons per day |
| gm | Grams | mL | Milliliter |
| gpd | Gallons per day | ppb | Parts per billion |
| gpg | Grains per gallon | ppm | Parts per million |
| gpm | Gallons per minute | psi | Pounds per square inch |
| gph | Gallons per hour | Q | Flow |
| gr | Grains | SS | Settleable solids |
| hp | Horsepower | TTHM | Total trihalomethanes |
| in | Inch | TOC | Total organic carbon |
| kg | Kilogram | TSS | Total suspended solids |
| kW | Kilowatt | VS | Volatile solids |
| kWh | Kilowatt-hour | W | Watt |

